## Analysis and Backcalculation for Pavement Structures



6<sup>th</sup> ICPT July 20-23 2008 Sapporo Japan

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- 1. Static Analysis
  - 1-1. Cylindrical coordinates
    - The Software GAMES is compared with BISAR
  - 1-2. Cartesian coordinates

• The uniform loads over a rectangular area and a circular area are compared

2. Dynamic Analysis

Wave propagation in viscoelastic multilayered media • The responses from the solutions are compared with the results of ADINA

3. Backcalculation

Dynamic backcalculation



Strain-Displacement

$$\begin{split} \varepsilon_r &= \frac{\partial u}{\partial r}; \quad \gamma_{r\theta} = \frac{1}{r} \frac{\partial u}{\partial \theta} + \frac{\partial v}{\partial r} - \frac{v}{r} \\ \varepsilon_\theta &= \frac{u}{r} + \frac{1}{r} \frac{\partial v}{\partial \theta}; \quad \gamma_{\theta z} = \frac{1}{r} \frac{\partial w}{\partial \theta} + \frac{\partial v}{\partial z} \\ \varepsilon_z &= \frac{\partial w}{\partial z}; \quad \gamma_{zr} = \frac{\partial w}{\partial r} + \frac{\partial u}{\partial z} \\ \end{array}$$

Strain-Stress

$$\varepsilon_{r} = \frac{1}{E} \left( \sigma_{r} - \nu \sigma_{\theta} - \nu \sigma_{z} \right); \quad \gamma_{r\theta} = \frac{2(1+\nu)}{E} \tau_{r\theta}$$
$$\varepsilon_{\theta} = \frac{1}{E} \left( \sigma_{\theta} - \nu \sigma_{z} - \nu \sigma_{r} \right); \quad \gamma_{\theta z} = \frac{2(1+\nu)}{E} \tau_{\theta z}$$
$$\varepsilon_{z} = \frac{1}{E} \left( \sigma_{z} - \nu \sigma_{r} - \nu \sigma_{\theta} \right); \quad \gamma_{zr} = \frac{2(1+\nu)}{E} \tau_{zr}$$

# Uniformly distributed circular load



## Features of GAMES

- Pavement: Multilayer pavement system with a possibility of interface slip.
- Surface load: Multiple vertical and/or horizontal circular loads.
- Analysis: Multiple points of interest.
- Response: Stresses, strains, and displacements

## 1. Static Analysis



1. Static Analysis

### **GAMES vs BISAR**

~ Distribution of horizontal displacement,  $u_x$  ~







1. Static Analysis



## **Interface Slip Models**

$$(1-\alpha_i)\left\{u_r^i(h_i)-u_r^{i+1}(0)\right\}=\alpha_i\beta_i\tau_{rz}^i(h_i)$$

Model 1(GAMES): 
$$\beta_i = b^* \left( \frac{1 + \nu_i}{E_i} + \frac{1 + \nu_{i+1}}{E_{i+1}} \right)$$

Model 2(BISAR) : 
$$\beta_i = 2b^* \left(\frac{1+\nu_i}{E_i}\right)$$

Model 3: 
$$\beta_i = 2b^* \sqrt{\left(\frac{1+\nu_i}{E_i}\right) \left(\frac{1+\nu_{i+1}}{E_{i+1}}\right)}$$

 $0 \le \alpha_i < 1.0$  slip parameter

GAMES vs BISAR (Interface slip) ~ Distribution of radial displacement, u ~



## GAMES vs BISAR (Interface slip) ~ Distribution of vertical displacement, w ~



## GAMES for Windows (graphics) ~ Features ~

Language: Japanese / English

- Unit of measurement: Load (kgf, kN), Length (cm), Elastic modulus (kgf/cm<sup>2</sup>, MPa)
- Input: Input of new parameters or import from existing file
- Output: analytical results and graphics visualization (contour and color fill plots) of strain

## GAMES for Windows ~ start-up window ~

■, - GAMES -	GAMES
	Subbase Subgrade
	Preferred Language © Japanese © English

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## GAMES for Windows ~ input window ~

🖼 - GAMES -	
ANALYSIS OF PAVEMENT	
1. SELECT FOLDER	
SEARCH C:¥	
2. UNITS OF MEASUREMENT	
INPUT: kgf, kgf/cm2, cm   OUTPUT: kgf/cm2, cm	
○ INPUT: kgf, kgf/cm2, cm  OUTPUT: MPa, cm	
O INPUT: kN, MPa, cm   OUTPUT: MPa, cm	
3. OBJECTIVE	
ANALYSIS ONLY     GRAPHICS	
HELP QUIT NEXT	

## GAMES for Windows ~ input window ~

🗑, - GAME5 -					
STRUCTURAL ANALYSIS OF		ENT BY M	ULTILAY		C THEORY
_ 1. DATA	<sub>□</sub> 2. INITIAL	SETTING			
C NEW DATA					
IMPORT FROM FILE	LAYERS		ADS	POINTS	
ODEN EU E		<u> </u>	2		
OPEN FILE					
3. LAYER PROPERTY		4. LOAD CHAF	RACTERISTIC -	<u></u>	
MODULUS(kgf/cm2) POISSON RATIO TH	HICKNESS(cm)	VERTIC	AL LOAD(kgf) RAI	DIUS (cm) X-AXIS (c	m) Y-AXIS(cm) HORI2
LAYER 2 81549.44 0.35	10.00	LOAD 2	2500.00	11.30 -10	.00 0.00
LAYER 3 4077.47 0.35 LAYER 4 2038.74 0.35	20.00				
LAYER 5 611.62 0.40					
	F	I			F
5. POINT OF INTEREST		-6. IN/001PU	I FILE		
LAYER         X-AXIS(cm)         Y-AXIS(cm)         Z-AXIS           POINT 1         1         0.00         0.00         1	(cm) 10.00				
POINT 2         1         16.00         0.00         1           POINT 3         2         0.00         0.00         2	20.00	analysis.dat	AM⊢	analysis-kgf.	Dut
POINT 4 2 16.00 0.00 2 POINT 5 5 0.00 0.00 2	20.00				
POINT 6         5         5.50         0.00         0	50.00				
			VI	EW RESULTS	
				,	
PREVIOUS CLEAR FORM	INPUT DATA OK!	SAVE IN	IPUT DATA	ANALYZE	HELP QUIT

## GAMES for Windows ~ output window ~

LATER PRI		
LAYER YOUN	IG'S POISSON'S THICKNESS SLIP	
(ksf)	(cm2) (cm)	
1 8154 2 8154	.9.44 0.35 10.00 0.00 .9.44 0.35 10.00 0.00	
0 403	7.47 0.35 20.00 0.00	
4 208 5 61	8.74 0.35 20.00 0.00 1.62 0.40	
==== TOTAL STR	ESS AND DISPLACEMENT RESULTS ====	
, Х., С., У.,	7 JIX JIV JIZ	
(cm) (cm) 0.00 0.0	(cm) (cm) (cm) (cm) 0 10.00 0.0000E+00 0.0000E+00 3.5388E-02	
16.00 0.0	0 I0.00 -2.3738E-05 0.0000E+00 3.4871E-02	
0.00 0.0 16.00 0.0	0	
0.00 0.0	0 \$0.00 0.0000E+00 0.0000E+00 2.\$670E-02	
16.00 0.0	0 \$0.00 1.882/2-08 0.00002+00 2.82662-02	
X Y (cm) (cm)	Z STRx STRy STRz (cm) (kgf/cm2) (kgf/cm2)	
0.00 0.0	0 10.00 -1.5977E+00 -3.3779E-01 -1.0784E+00	
0.00 0.0	0 10.00 -8.1203E-01 -8.7713E-01 -3.8134E+00 10 20.00 6.1608E+00 8.4320E+00 -5.6111E-01	
16.00 0.0	.0 20.00 7.1537E+00 8.5229E+00 -5.8406E-01	
16.00 0.0	0 60.00 -1.0079E-03 3.7960E-03 -1.2684E-01	
х ү	Z STRxy STRxz STRyz	
(cm) (cm)	(cm) (kgf/cm2) (kgf/cm2) (kgf/cm2)	
16.00 0.0	0 I0.00 0.0000E+00 -6.2920E-01 0.0000E+00	
0.00 0.0 16.00 0.0	0 20.00 0.0000E+00 0.0000E+00 0.0000E+00 0 20.00 0.0000E+00 -1.2883E-01 0.0000E+00	
0.00 0.0	0 \$0.00 0.0000E+00 0.0000E+00 0.0000E+00	
16.00 0.0	0 60.00 0.0000E+00 -1.5702E-02 0.0000E+00	
X Y (cm) (cm)	Z EPSx EPSy EPSz	

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## GAMES for Windows ~ input window ~

🐃 – GAMES –	
ANALYSIS OF PAVEMENT	
1. SELECT FOLDER SEARCH	
<ul> <li>2. UNITS OF MEASUREMENT</li> <li>INPUT: kgf, kgf/cm2, cm   OUTPUT: kgf/cm2, cm</li> </ul>	
© INPUI: kgt, kgt/cm2, cm   OUIPUI: MPa, cm © INPUT: kN, MPa, cm   OUTPUT: MPa, cm	
3. OBJECTIVE • ANALYSIS ONLY • GRAPHICS	
HELP OHIT NFXT	
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## GAMES for Windows ~ input window ~

🖷 – GAMES –		
INITIAL SETTI	NG FOR GRAPHICS PRESENTATIO	N
I. DATA	2. INITIAL SETTING	INPUT FILENAME
O NEW DATA		
• IMPORT FROM FILE	LAYERS LOADS	graphics dat
OPEN ETLE		graphics.uur
OT ENTIRE		
_3. LAYER I	ROPERTY	
	ODULUS(kgf/cm2) POISSON RATIO THICKNESS(cm) SL	
LATER 1 LAYER 2	81549.44         0.35         10.00           81549.44         0.35         10.00	
LAYER 3 LAYER 4	4077.47 0.35 20.00 2038.74 0.35 20.00	
LAYER 5	611.62 0.40	
	-	
<b>□ 4. LOAD CHARACTERIST</b>	c	
VERTICAL LOAD(k	f) RADIUS(cm) X-AXIS(cm) Y-AXIS(cm) HORIZONTAL LO	AD(kgf) ANGL
LOAD 1 5000.	0 15.00 0.00 0.00	0.00
PREVIOUS CLEAR FORM	PUT DATA OK! SAVE INPUT DATA GUTO GRAPHICS	HELP QUIT
Oth LOT		

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## **GAMES** for Windows ~ output window ~

R, GAMES				_ □
T. INITIAL SETTING		_		
EPSx	C EPSz			
L		_		
2. X-SECTION				
• X-Y SECTION	SECTION SECTION	35.0		GAMES_VB.CSV
POSITION(Z-SECT.(c)	m)) 20	9.04E-5		( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (
<u> </u>				
DATA FOR ANALYSIS	S. MIN/WAX VALUES			
	MIN. VALUE MAX. VALU	E 17.5 - 4.62E-5		
ANALYZE	Y-AXIS -35.0 35.0			
	VALUE 1.89DE-6 9.044E-5	<b>1.89E-6</b>		
DATA FOR GRAPHIDS				
	-   _4. D'SPLAY ITEM	0.0 - 3	9.05-5	
READ DATA	CONTOUR (COLORFILL)			
	CONTOUR (LINE)			
PLOT GRAPHICS	EGEND			$(HH)$ $(\Lambda \Lambda \Lambda)$
		-17.5 - / / / /		
CLEAR FORM				
		-351		
QUIT		-35.0	-17.5 0.0	17.5 35.0
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Summary and recommendations **Computational accuracy of GAMES** Accuracy of GAMES is similar to and in some cases better than BISAR. User interface and visualization process Improves efficiency in the use of GAMES and assists users to visualize distribution of pavement responses. Application GAMES can be used for analysis. evaluation and design of pavements.

## Dual Tire Footprints by SIM (Stress In Motion) (measured at CSIR, South Africa)



### 30 kN & 420 kPa inflation pressure

# 70 kN & 420 kPa inflation pressure

### Contact pressure measured by SIM (provided by Prof. Morris De Beer)

WIDE BASE TYRE LOAD IN X DIRECTION - DECIMATED DATA (75 kN and 500 kPa)



#### Contact pressure measured by SIM (provided by Prof. Morris De Beer)



WIDE BASE TYRE LOAD IN Y DIRECTION - DECIMATED DATA (75 kN and 500 kPa)

### Contact pressure measured by SIM (provided by Prof. Morris De Beer)

WIDE BASE TYRE LOAD IN Z DIRECTION - DECIMATED DATA (75 kN and 500 kPa)



### 1. Static Analysis in the Cartesian Coordinate Equilibrium $\frac{\partial \sigma_x}{\partial x} + \frac{\partial \tau_{xy}}{\partial y} + \frac{\partial \tau_{xz}}{\partial z} = 0$ dx $\frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \sigma_y}{\partial y} + \frac{\partial \tau_{zy}}{\partial z} = 0$ dy $\frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \sigma_{z}}{\partial z} = 0$ dz. Strain-displacement $\sigma_{y} + \frac{\partial \sigma_{y}}{\partial y} dy$ $\varepsilon_x = \frac{\partial u}{\partial x}; \quad \varepsilon_y = \frac{\partial v}{\partial y}; \quad \varepsilon_z = \frac{\partial w}{\partial z}$ $\tau_{xz} + \frac{\partial \tau_{xz}}{\partial x} dx$ $\frac{\partial \tau_{zx}}{\partial z} dz$ $\gamma_{xy} = \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y}; \quad \gamma_{yz} = \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z}; \quad \gamma_{zx} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \qquad \qquad \tau_{yz} + \frac{\partial \tau_{yz}}{\partial y} \frac{dy}{\tau_{zy}} + \frac{\partial \tau_{zy}}{\partial z} \frac{dz}{dz} + \frac{\partial \sigma_{z}}{\partial z} \frac{dz}{dz}$ **Strain-stress** $\varepsilon_x = \frac{1}{E} (\sigma_x - v\sigma_y - v\sigma_z); \gamma_{xy} = \frac{2(1+v)}{E} \tau_{xy}$ $\varepsilon_{y} = \frac{1}{E} \left( \sigma_{y} - \nu \sigma_{z} - \nu \sigma_{x} \right); \gamma_{yz} = \frac{2(1+\nu)}{E} \tau_{yz}$ $\varepsilon_{z} = \frac{1}{E} \left( \sigma_{z} - \nu \sigma_{x} - \nu \sigma_{y} \right); \gamma_{zx} = \frac{2(1+\nu)}{E} \tau_{zx}$ 6th ICPT July 20-23 2008 Sapporo Japan No.26

## Method of Solution

# **Neuber-Papkovich Representation** $u = \frac{1}{2\mu} B_x - \frac{\lambda + \mu}{4\mu(\lambda + 2\mu)} \frac{\partial}{\partial x} \left( xB_x + yB_y + zB_z \right)$ $v = \frac{1}{2\mu}B_{y} - \frac{\lambda + \mu}{4\mu(\lambda + 2\mu)}\frac{\partial}{\partial y}\left(xB_{x} + yB_{y} + zB_{z}\right)$ $w = \frac{1}{2\mu}B_z - \frac{\lambda + \mu}{4\mu(\lambda + 2\mu)}\frac{\partial}{\partial z}\left(xB_x + yB_y + zB_z\right)$ where $\nabla^2 B_x(x, y, z) = \nabla^2 B_y(x, y, z) = \nabla^2 B_z(x, y, z) = 0$

## 1. Static Analysis

### Rectangular Area vs Circular Area



## 1. Static Analysis

### Rectangular Area vs Circular Area



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~ Dual tires ~



## Non-uniform Surface Loading





# Dynamic Analysis of Pavement Structure



## 2. Dynamic Analysis

2-1. Axi-symmetric wave propagation analysis

$$\frac{\partial \sigma_r}{\partial r} + \frac{\partial \tau_{rz}}{\partial z} + \frac{\sigma_r - \sigma_{\theta}}{r} = \frac{\partial^2 u}{\partial t^2}$$
$$\frac{\partial \tau_{rz}}{\partial r} + \frac{\partial \sigma_z}{\partial z} + \frac{\tau_{rz}}{r} = \frac{\partial^2 w}{\partial t^2}$$



### Stress-Strain

$$\begin{cases} \sigma_r \\ \sigma_\theta \\ \sigma_z \\ \tau_{rz} \end{cases} = E \begin{pmatrix} a+2b & a & a & 0 \\ a & a+2b & a & 0 \\ a & a & a+2b & 0 \\ 0 & 0 & 0 & b \end{pmatrix} \begin{cases} \varepsilon_r \\ \varepsilon_\theta \\ \varepsilon_z \\ \gamma_{rz} \end{cases}$$
$$= \frac{\nu}{(1+\nu)(1-2\nu)} \quad b = \frac{1}{2(1+\nu)}$$

**FEM** formulation

$$\begin{bmatrix} M \end{bmatrix} \{ \ddot{z} \} + \begin{bmatrix} K \end{bmatrix} \{ z \} = \{ f \} \\ \bigcup \\ \begin{bmatrix} M \end{bmatrix} \{ \ddot{z} \} + \begin{bmatrix} C \end{bmatrix} \{ \dot{z} \} + \begin{bmatrix} K \end{bmatrix} \{ z \} = \{ f \} \\ \begin{bmatrix} C \end{bmatrix} = \beta \begin{bmatrix} K \end{bmatrix} \\ \end{bmatrix}$$
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#### 2. Dynamic Analysis

#### Wave-Pave, Dyna-Pave vs. ADINA



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2. Dynamic Analysis



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# Summary

 Dynamic analysis with stiffness proportional damping is equivalent to dynamic analysis with the Kelvin model



#### 2. Dynamic Analysis

• Wave-Pave



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# **Dynamic Backcalculation**

D-BALM (FEM)

W-BALM(Wave-Pave)

**BALM: Static Backcalculation** 

#### Backcalculation

#### **Objective Function**

$$J = \frac{1}{2LN} \sum_{\ell=1}^{L} \int_{t0}^{t1} \sum_{i=1}^{N} \left\{ u_i^{(\ell)}(t) - z_i^{(\ell)}(\mathbf{X}, t) \right\}^2 dt$$

L: Number of tests

N: Number of sensors



**X** Vector of unknown parameters

(layer modulus and layer damping)

 $(t_0, t_1)$  Time interval of deflection matching

#### National Institute for Land and Infrastructure Management (NILIM) in Japan



Same Size as Landing Gear of B747-400 Max. Running Speed : 5km/h Max. Load : 1200kN







Test Condition Running Speed : 5km/h Load : 910kN Load Repetition : 10,000 times

Measurement Item Dynamic Vertical Displacement Dynamic Soil Pressure

Aircraft Load Simulator

## **Backcalculated Results E1&C1**



## **Backcalculated Results E2&C2**





#### **Backcalculated Results E3&C3**



#### Incorporated Administrative Agency Public Works Research Institute Civil Engineering Research Institute for Cold Region (CERI)



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# **CERI Field Test Site**



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# City of Wakkanai



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#### **Pavement Cross Sections**



測点	P=1870∼1950	P=2080∼2160	P=2160∼2240	P=2240~2320	P=2483.5 ~2493.5	P=2493. 5∼2523. 5	P=2523.5 ~2530	P=2530∼2560	P=2560∼ 2570	P=2570∼2600
延長	L=80	L=80	L=80	L=80	L=10	L=30	L=6.5	L=30	L=10	L=30

※As層厚および路盤厚は、㈱ウオールナットさんの実測値を使用した。 ただし、センサー設置位置は路盤上部が多少下がっていると 予想して、路線調査におけるセンサー設置測点の舗装厚から、センサー位置JustにおけるAs層厚を差し引いたものを路盤厚とした。 ※路床厚は調査で測定できなかったことから、従来どおり地質断面図から推定した。

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## **FWD** Test



National highway 238 (test site)

## **Truck Loading Test**



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#### **Position of FWD Loading Plate**























August 2006


## **Questions** ?

GAMES can be downloaded from

http://www.jsce.or.jp/committee/pavement/downloads/ http://matsui.labo.googlepages.com/games\_win.eng

Thank you !

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1. Static Analysis

## GAMES vs BISAR

~ Distribution of shearing stress,  $t_{xz}$  ~



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Dynamic Back-calculation using FWD Deflection Data

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